



MODELLING AND NUMERICAL SIMULATION OF BIOCHEMICAL-OXYGEN DEMAND AND DISSOLVED-OXYGEN INTERACTIONS DUE TO POLLUTION IN RIVER GANGES

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ABSTRACT

In effluents discharge modelling, we have investigated the impact of temperature variation (Increasing Temperature, $T=28$ unit) in the interaction between Biochemical-Oxygen Demand (BOD) and Dissolved Oxygen (DO) on a polluted river Ganges. Here, we have derived first an analytical solution that can predict the relative abundance of both coordinates in their interaction at any time, t . Furthermore, a numerical scheme of Runge-Kutta ODE45 computational approach was used to study the qualitative characteristics of the BOD-DO interaction for the impact of temperature variation (Increasing Temperature @ $T=28$ unit) in the interaction between BOD (IC = 8.0) and DO (IC = 7.1) at an interval of 0(0.1)60 time in hrs, when all model parameter values are fixed ranging from the time interval of 0:0.1:60 in hrs. The BOD and DO initial values here called the IC's on the base time recorded as $BOD_0 = 8.0$ and $DO_0 = 7.1$ due to the pollution of the stream. Furthermore, from the base time, we observed a severe depletion of the DO downstream from a value of 7.1 units DO to a value of 4.0099 units DO for the uncontrol coordinate and 4.4353unit DO for the control (Modified) coordinate at 1.7hr of our experimental time which further recover with various DO deficit up to full saturation. The detail work and full results are presented and discussed in this study.

Keywords: Biochemical-Oxygen Demand, Dissolved Oxygen, Numerical Simulation, Biological Extinction, Model Parameters.

INTRODUCTION

The Oxford dictionary defines pollution as “the presence in or introduction into the environment of a substance which has harmful or poisonous effect. There are many types of pollution including air pollution, water pollution, land pollution, radioactive pollution and thermal pollution” (oxford dictionaries.com).

One of the major types of environmental pollution is water pollution of which the River Ganges is being highly polluted on a daily basis. Water the most important constituent for existence of life on earth is being polluted every day and its aquatic species existence and survival are

vulnerable to biological extinction. This has become an increasing and challenging problem in environmental management and ecosystem functioning globally. The water bodies become polluted due to untreated waste, sewage, agricultural discharge and toxic metals. The effect of this is that the pollutants impart colour, taste, and odour, to receiving water thus making it unfit for use. The most challenging problem in the society is the change in the environment caused by the pollution affecting the long-term survival of the aquatic species, human lifestyle and bio-diversity of the habitat. A great quantity of toxicants and contaminants enters into the River Ganges continuously which threaten the survival of the exposed population including human beings. This challenging environmental problem will be solve computationally using numerical simulation approach (Akpodee and Ekaka-a,2019) on an interacting Dissolved-Oxygen and Bio-Oxygen Demand on the polluted river for water quality and aquatic species survival.

MATHEMATICAL FORMULATION

When water of river is polluted then the river has an ability to purify itself using some chemical and biological actions. This is known as self-purification. Self-purification can be proved as a good indicator for the status of a river, whenever pollutants is there in a river; 2 process takes place simultaneously.

1. De-oxygen
2. Re-aeration

Due to these processes, river has its self-cleansing property.

We will consider now the case of first-order decay equation of industrial wastes. Equation for two processes is as follows (Kaushik, 2015):

$$\begin{aligned}\dot{X} &= -DC^\tau Y + KT_c^\tau (S - X) \\ \dot{Y} &= -DC^\tau Y\end{aligned}$$

D = decay rate/day

K = proportional coefficient

C = correction coefficient

$$\tau = T - 20$$

X =Dissolved Oxygen (D.O); Y =Biochemical-Oxygen Demand (B.O.D).

T_c = temperature correction coefficient

S = saturation concentration

Thus, the predictive model for dissolved oxygen (DO) and Bio-oxygen Demand (BOD) for an arbitrary parameter values are stated as follows

$$\begin{aligned}X(t) &= S + \frac{DC^\tau y_0}{(DC^\tau - KT_c^\tau)} \cdot e^{-(DC^\tau)t} + \left(X_0 - S - \frac{DC^\tau y_0}{(DC^\tau - KT_c^\tau)} \right) e^{-KT_c^\tau t} \\ Y(t) &= y_0 e^{-DC^\tau t}\end{aligned}$$

METHOD OF SOLUTION

Using the Data set: (Data source: Rajat Kaushik, 2015)

$$D = 0.3 \text{ Day}^{-1}$$

$$K = 0.1 \text{ Day}^{-1}$$

$$C = 1.048 \text{ Day}^{-1}$$

$$T = 24^{\circ}\text{C}$$

$$\tau = T - 20 = (24 - 20)^{\circ}\text{C}$$

$$S = 8.3374 \text{ mg/L}$$

$$X_0 = 7.1 \text{ mg/L} \quad \text{at } t = 0$$

$$y_0 = 8.0 \text{ mg/L} \quad \text{at } t = 0$$

$$T_c = 1.0300$$

Substituting the parameter into the solution map and evaluating. We have,

$$X(t) = 8.3374 + \left[\frac{(0.3)(1.048^4)(8.0)}{(0.3)(1.048^4) - (0.1)(1.03^4)} \right] e^{-(0.3)(1.048^4)t} + 7.1 - 8.3374$$

$$- \left[\frac{(0.3)(1.048^4)(8.0)}{(0.3)(1.048^4) - (0.1)(1.03^4)} \right] e^{-(0.1)(1.03^4)t}$$

$$X(t) = 8.3374 + \left[\frac{(2.895052023)}{(0.36188 - 0.112550881)} \right] e^{-(0.36188)t} + 7.1 - 8.3374$$

$$- \left[\frac{(2.895052023)}{(0.36188) - (0.112550881)} \right] e^{-(0.11255088)t}$$

$$X(t) = 8.3374 + \left[\frac{(2.895052023)}{(0.24932912)} \right] e^{-(0.36188)t} + 7.1 - 8.3374$$

$$- \left[\frac{(2.895052023)}{(0.24932912)} \right] e^{-(0.11255088)t}$$

$$X(t) = 8.3374 + 11.6113674e^{-(0.36188)t} + (7.1 - 8.3374$$

$$- 11.61136743)e^{-(0.11255088)t}$$

$$X(t) = 8.3374 + 11.6113674e^{-(0.36188)t} - 12.84876e^{-(0.11255088)t}$$

The requirement solution trajectory of the DO and BOD on the polluted water Gange in thus states as:

$$X(t) = 8.3374 + 11.6113674e^{-(0.36188)t} - 12.84876e^{-(0.11255088)t}$$

$$Y(t) = 8.0e^{-0.36188t}$$

The numerical simulation aspects using the above solution trajectories of the BOD-DO model will be the core of this studies.

Results and Discussion

Table1: Impact of Temperature Gradient on Self Purification of an Industrial Polluted Water Ganges

| Time | DO | DO _m | BOD | BOD _m |
|--------|--------|-----------------|--------|------------------|
| 0 | 7.1000 | 7.1000 | 8.0000 | 8.0000 |
| 0.1000 | 6.8311 | 6.7760 | 7.7157 | 7.6583 |
| 0.2000 | 6.5753 | 6.4707 | 7.4414 | 7.3312 |
| 0.3000 | 6.3320 | 6.1830 | 7.1770 | 7.0180 |
| 0.4000 | 6.1008 | 5.9123 | 6.9219 | 6.7183 |
| 0.5000 | 5.8813 | 5.6576 | 6.6759 | 6.4313 |
| 0.6000 | 5.6728 | 5.4184 | 6.4386 | 6.1566 |
| 0.7000 | 5.4750 | 5.1937 | 6.2097 | 5.8935 |
| 0.8000 | 5.2874 | 4.9829 | 5.9889 | 5.6416 |
| 0.9000 | 5.1095 | 4.7853 | 5.7758 | 5.4004 |
| 1.0000 | 4.9412 | 4.6004 | 5.5703 | 5.1694 |
| 1.1000 | 4.7820 | 4.4277 | 5.3720 | 4.9483 |
| 1.2000 | 4.6316 | 4.2665 | 5.1809 | 4.7367 |
| 1.3000 | 4.4897 | 4.1165 | 4.9966 | 4.5343 |
| 1.4000 | 4.3559 | 3.9771 | 4.8188 | 4.3405 |
| 1.5000 | 4.2301 | 3.8478 | 4.6475 | 4.1551 |
| 1.6000 | 4.1117 | 3.7281 | 4.4822 | 3.9777 |
| 1.7000 | 4.0007 | 3.6175 | 4.3230 | 3.8080 |
| 1.8000 | 3.8965 | 3.5156 | 4.1694 | 3.6456 |
| 1.9000 | 3.7991 | 3.4220 | 4.0214 | 3.4901 |
| 2.0000 | 3.7080 | 3.3361 | 3.8786 | 3.3413 |
| 2.1000 | 3.6231 | 3.2576 | 3.7410 | 3.1989 |
| 2.2000 | 3.5440 | 3.1860 | 3.6083 | 3.0624 |
| 2.3000 | 3.4704 | 3.1210 | 3.4803 | 2.9317 |
| 2.4000 | 3.4022 | 3.0622 | 3.3568 | 2.8064 |
| 2.5000 | 3.3391 | 3.0094 | 3.2376 | 2.6865 |
| 2.6000 | 3.2808 | 2.9623 | 3.1227 | 2.5716 |
| 2.7000 | 3.2270 | 2.9207 | 3.0117 | 2.4617 |
| 2.8000 | 3.1777 | 2.8842 | 2.9046 | 2.3564 |
| 2.9000 | 3.1327 | 2.8527 | 2.8013 | 2.2557 |
| 3.0000 | 3.0918 | 2.8260 | 2.7017 | 2.1593 |
| 3.1000 | 3.0549 | 2.8037 | 2.6056 | 2.0670 |
| 3.2000 | 3.0218 | 2.7856 | 2.5129 | 1.9788 |
| 3.3000 | 2.9924 | 2.7716 | 2.4235 | 1.8943 |
| 3.4000 | 2.9665 | 2.7613 | 2.3373 | 1.8134 |
| 3.5000 | 2.9439 | 2.7547 | 2.2542 | 1.7361 |
| 3.6000 | 2.9246 | 2.7514 | 2.1740 | 1.6620 |
| 3.7000 | 2.9084 | 2.7514 | 2.0968 | 1.5911 |
| 3.8000 | 2.8951 | 2.7543 | 2.0223 | 1.5233 |

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|--------|--------|--------|--------|--------|
| 3.9000 | 2.8846 | 2.7600 | 1.9505 | 1.4583 |
| 4.0000 | 2.8768 | 2.7683 | 1.8812 | 1.3960 |
| 4.1000 | 2.8715 | 2.7791 | 1.8144 | 1.3363 |
| 4.2000 | 2.8687 | 2.7923 | 1.7500 | 1.2792 |
| 4.3000 | 2.8682 | 2.8077 | 1.6879 | 1.2245 |
| 4.4000 | 2.8699 | 2.8252 | 1.6280 | 1.1721 |
| 4.5000 | 2.8736 | 2.8448 | 1.5702 | 1.1220 |
| 4.6000 | 2.8793 | 2.8663 | 1.5144 | 1.0740 |
| 4.7000 | 2.8869 | 2.8895 | 1.4606 | 1.0281 |
| 4.8000 | 2.8962 | 2.9144 | 1.4087 | 0.9842 |
| 4.9000 | 2.9073 | 2.9409 | 1.3586 | 0.9422 |
| 5.0000 | 2.9200 | 2.9689 | 1.3102 | 0.9019 |
| 5.1000 | 2.9342 | 2.9983 | 1.2636 | 0.8635 |
| 5.2000 | 2.9499 | 3.0289 | 1.2186 | 0.8266 |
| 5.3000 | 2.9671 | 3.0607 | 1.1753 | 0.7914 |
| 5.4000 | 2.9856 | 3.0937 | 1.1335 | 0.7577 |
| 5.5000 | 3.0054 | 3.1276 | 1.0932 | 0.7253 |
| 5.6000 | 3.0264 | 3.1624 | 1.0543 | 0.6944 |
| 5.7000 | 3.0486 | 3.1981 | 1.0168 | 0.6647 |
| 5.8000 | 3.0719 | 3.2346 | 0.9807 | 0.6363 |
| 5.9000 | 3.0962 | 3.2718 | 0.9459 | 0.6091 |
| 6.0000 | 3.1215 | 3.3096 | 0.9123 | 0.5831 |
| 6.1000 | 3.1477 | 3.3481 | 0.8799 | 0.5581 |
| 6.2000 | 3.1748 | 3.3872 | 0.8487 | 0.5342 |
| 6.3000 | 3.2026 | 3.4268 | 0.8186 | 0.5114 |
| 6.4000 | 3.2313 | 3.4668 | 0.7895 | 0.4895 |
| 6.5000 | 3.2606 | 3.5073 | 0.7615 | 0.4686 |
| 6.6000 | 3.2905 | 3.5483 | 0.7345 | 0.4486 |
| 6.7000 | 3.3211 | 3.5895 | 0.7084 | 0.4294 |
| 6.8000 | 3.3521 | 3.6311 | 0.6832 | 0.4111 |
| 6.9000 | 3.3838 | 3.6729 | 0.6589 | 0.3936 |
| 7.0000 | 3.4159 | 3.7150 | 0.6355 | 0.3768 |
| 7.1000 | 3.4484 | 3.7572 | 0.6128 | 0.3608 |
| 7.2000 | 3.4815 | 3.7996 | 0.5910 | 0.3454 |
| 7.3000 | 3.5149 | 3.8421 | 0.5700 | 0.3307 |
| 7.4000 | 3.5487 | 3.8847 | 0.5497 | 0.3166 |
| 7.5000 | 3.5828 | 3.9273 | 0.5301 | 0.3030 |
| 7.6000 | 3.6172 | 3.9700 | 0.5113 | 0.2901 |
| 7.7000 | 3.6520 | 4.0126 | 0.4931 | 0.2777 |
| 7.8000 | 3.6870 | 4.0553 | 0.4756 | 0.2658 |
| 7.9000 | 3.7223 | 4.0978 | 0.4587 | 0.2544 |
| 8.0000 | 3.7577 | 4.1404 | 0.4424 | 0.2436 |
| 8.1000 | 3.7934 | 4.1829 | 0.4267 | 0.2331 |
| 8.2000 | 3.8292 | 4.2253 | 0.4115 | 0.2232 |

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|---------|--------|--------|--------|--------|
| 8.3000 | 3.8651 | 4.2675 | 0.3970 | 0.2136 |
| 8.4000 | 3.9012 | 4.3097 | 0.3829 | 0.2045 |
| 8.5000 | 3.9374 | 4.3517 | 0.3693 | 0.1958 |
| 8.6000 | 3.9736 | 4.3936 | 0.3562 | 0.1874 |
| 8.7000 | 4.0099 | 4.4353 | 0.3436 | 0.1794 |
| 8.8000 | 4.0462 | 4.4768 | 0.3314 | 0.1718 |
| 8.9000 | 4.0825 | 4.5182 | 0.3196 | 0.1645 |
| 9.0000 | 4.1189 | 4.5593 | 0.3082 | 0.1575 |
| 9.1000 | 4.1552 | 4.6002 | 0.2973 | 0.1507 |
| 9.2000 | 4.1914 | 4.6408 | 0.2867 | 0.1443 |
| 9.3000 | 4.2277 | 4.6812 | 0.2765 | 0.1382 |
| 9.4000 | 4.2639 | 4.7214 | 0.2666 | 0.1322 |
| 9.5000 | 4.3000 | 4.7613 | 0.2572 | 0.1266 |
| 9.6000 | 4.3361 | 4.8009 | 0.2480 | 0.1212 |
| 9.7000 | 4.3721 | 4.8403 | 0.2392 | 0.1160 |
| 9.8000 | 4.4080 | 4.8794 | 0.2307 | 0.1110 |
| 9.9000 | 4.4439 | 4.9182 | 0.2225 | 0.1063 |
| 10.0000 | 4.4796 | 4.9567 | 0.2146 | 0.1017 |
| 10.1000 | 4.5152 | 4.9949 | 0.2069 | 0.0974 |
| 10.2000 | 4.5507 | 5.0329 | 0.1996 | 0.0932 |
| 10.3000 | 4.5860 | 5.0705 | 0.1925 | 0.0892 |
| 10.4000 | 4.6212 | 5.1079 | 0.1857 | 0.0854 |
| 10.5000 | 4.6562 | 5.1449 | 0.1791 | 0.0818 |
| 10.6000 | 4.6911 | 5.1816 | 0.1727 | 0.0783 |
| 10.7000 | 4.7259 | 5.2180 | 0.1666 | 0.0750 |
| 10.8000 | 4.7604 | 5.2541 | 0.1607 | 0.0718 |
| 10.9000 | 4.7948 | 5.2899 | 0.1550 | 0.0687 |
| 11.0000 | 4.8290 | 5.3254 | 0.1495 | 0.0658 |
| 11.1000 | 4.8629 | 5.3605 | 0.1442 | 0.0630 |
| 11.2000 | 4.8967 | 5.3953 | 0.1391 | 0.0603 |
| 11.3000 | 4.9303 | 5.4298 | 0.1341 | 0.0577 |
| 11.4000 | 4.9637 | 5.4639 | 0.1293 | 0.0552 |
| 11.5000 | 4.9969 | 5.4977 | 0.1247 | 0.0529 |
| 11.6000 | 5.0298 | 5.5312 | 0.1203 | 0.0506 |
| 11.7000 | 5.0626 | 5.5644 | 0.1160 | 0.0485 |
| 11.8000 | 5.0951 | 5.5972 | 0.1119 | 0.0464 |
| 11.9000 | 5.1275 | 5.6298 | 0.1079 | 0.0444 |
| 12.0000 | 5.1596 | 5.6620 | 0.1041 | 0.0425 |
| 12.1000 | 5.1915 | 5.6938 | 0.1004 | 0.0407 |
| 12.2000 | 5.2231 | 5.7254 | 0.0968 | 0.0390 |
| 12.3000 | 5.2546 | 5.7566 | 0.0934 | 0.0373 |
| 12.4000 | 5.2858 | 5.7875 | 0.0901 | 0.0357 |
| 12.5000 | 5.3168 | 5.8181 | 0.0869 | 0.0342 |
| 12.6000 | 5.3475 | 5.8484 | 0.0838 | 0.0327 |

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|---------|--------|--------|--------|--------|
| 12.7000 | 5.3780 | 5.8783 | 0.0808 | 0.0313 |
| 12.8000 | 5.4083 | 5.9079 | 0.0779 | 0.0300 |
| 12.9000 | 5.4383 | 5.9373 | 0.0752 | 0.0287 |
| 13.0000 | 5.4681 | 5.9663 | 0.0725 | 0.0275 |
| 13.1000 | 5.4977 | 5.9949 | 0.0699 | 0.0263 |
| 13.2000 | 5.5270 | 6.0233 | 0.0675 | 0.0252 |
| 13.3000 | 5.5561 | 6.0514 | 0.0651 | 0.0241 |
| 13.4000 | 5.5849 | 6.0791 | 0.0627 | 0.0231 |
| 13.5000 | 5.6135 | 6.1066 | 0.0605 | 0.0221 |
| 13.6000 | 5.6418 | 6.1337 | 0.0584 | 0.0211 |
| 13.7000 | 5.6699 | 6.1605 | 0.0563 | 0.0202 |
| 13.8000 | 5.6978 | 6.1871 | 0.0543 | 0.0194 |
| 13.9000 | 5.7254 | 6.2133 | 0.0523 | 0.0185 |
| 14.0000 | 5.7528 | 6.2393 | 0.0505 | 0.0178 |
| 14.1000 | 5.7799 | 6.2649 | 0.0487 | 0.0170 |
| 14.2000 | 5.8068 | 6.2903 | 0.0470 | 0.0163 |
| 14.3000 | 5.8335 | 6.3154 | 0.0453 | 0.0156 |
| 14.4000 | 5.8599 | 6.3402 | 0.0437 | 0.0149 |
| 14.5000 | 5.8861 | 6.3647 | 0.0421 | 0.0143 |
| 14.6000 | 5.9120 | 6.3889 | 0.0406 | 0.0137 |
| 14.7000 | 5.9378 | 6.4129 | 0.0392 | 0.0131 |
| 14.8000 | 5.9632 | 6.4365 | 0.0378 | 0.0125 |
| 14.9000 | 5.9885 | 6.4599 | 0.0365 | 0.0120 |
| 15.0000 | 6.0135 | 6.4831 | 0.0352 | 0.0115 |
| 15.1000 | 6.0383 | 6.5059 | 0.0339 | 0.0110 |
| 15.2000 | 6.0628 | 6.5285 | 0.0327 | 0.0105 |
| 15.3000 | 6.0871 | 6.5508 | 0.0316 | 0.0101 |
| 15.4000 | 6.1112 | 6.5729 | 0.0304 | 0.0096 |
| 15.5000 | 6.1350 | 6.5947 | 0.0294 | 0.0092 |
| 15.6000 | 6.1586 | 6.6162 | 0.0283 | 0.0088 |
| 15.7000 | 6.1820 | 6.6375 | 0.0273 | 0.0085 |
| 15.8000 | 6.2052 | 6.6586 | 0.0263 | 0.0081 |
| 15.9000 | 6.2281 | 6.6793 | 0.0254 | 0.0077 |
| 16.0000 | 6.2508 | 6.6999 | 0.0245 | 0.0074 |
| 16.1000 | 6.2733 | 6.7202 | 0.0236 | 0.0071 |
| 16.2000 | 6.2955 | 6.7402 | 0.0228 | 0.0068 |
| 16.3000 | 6.3176 | 6.7601 | 0.0220 | 0.0065 |
| 16.4000 | 6.3394 | 6.7796 | 0.0212 | 0.0062 |

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|---------|--------|--------|--------|--------|
| 16.5000 | 6.3610 | 6.7990 | 0.0204 | 0.0060 |
| 16.6000 | 6.3824 | 6.8181 | 0.0197 | 0.0057 |
| 16.7000 | 6.4036 | 6.8370 | 0.0190 | 0.0055 |
| 16.8000 | 6.4246 | 6.8556 | 0.0183 | 0.0052 |
| 16.9000 | 6.4453 | 6.8741 | 0.0177 | 0.0050 |
| 17.0000 | 6.4659 | 6.8923 | 0.0171 | 0.0048 |
| 17.1000 | 6.4862 | 6.9103 | 0.0164 | 0.0046 |
| 17.2000 | 6.5064 | 6.9280 | 0.0159 | 0.0044 |
| 17.3000 | 6.5263 | 6.9456 | 0.0153 | 0.0042 |
| 17.4000 | 6.5460 | 6.9629 | 0.0148 | 0.0040 |
| 17.5000 | 6.5656 | 6.9801 | 0.0142 | 0.0039 |
| 17.6000 | 6.5849 | 6.9970 | 0.0137 | 0.0037 |
| 17.7000 | 6.6040 | 7.0137 | 0.0132 | 0.0035 |
| 17.8000 | 6.6230 | 7.0302 | 0.0128 | 0.0034 |
| 17.9000 | 6.6417 | 7.0465 | 0.0123 | 0.0032 |
| 18.0000 | 6.6602 | 7.0626 | 0.0119 | 0.0031 |
| 18.1000 | 6.6786 | 7.0785 | 0.0115 | 0.0030 |
| 18.2000 | 6.6968 | 7.0943 | 0.0110 | 0.0028 |
| 18.3000 | 6.7147 | 7.1098 | 0.0107 | 0.0027 |
| 18.4000 | 6.7325 | 7.1251 | 0.0103 | 0.0026 |
| 18.5000 | 6.7501 | 7.1403 | 0.0099 | 0.0025 |
| 18.6000 | 6.7675 | 7.1552 | 0.0096 | 0.0024 |
| 18.7000 | 6.7848 | 7.1700 | 0.0092 | 0.0023 |
| 18.8000 | 6.8018 | 7.1846 | 0.0089 | 0.0022 |
| 18.9000 | 6.8187 | 7.1990 | 0.0086 | 0.0021 |
| 19.0000 | 6.8354 | 7.2133 | 0.0083 | 0.0020 |
| 19.1000 | 6.8519 | 7.2273 | 0.0080 | 0.0019 |
| 19.2000 | 6.8682 | 7.2412 | 0.0077 | 0.0018 |
| 19.3000 | 6.8844 | 7.2550 | 0.0074 | 0.0018 |
| 19.4000 | 6.9004 | 7.2685 | 0.0072 | 0.0017 |
| 19.5000 | 6.9162 | 7.2819 | 0.0069 | 0.0016 |
| 19.6000 | 6.9319 | 7.2951 | 0.0067 | 0.0015 |
| 19.7000 | 6.9474 | 7.3082 | 0.0064 | 0.0015 |
| 19.8000 | 6.9627 | 7.3211 | 0.0062 | 0.0014 |
| 19.9000 | 6.9779 | 7.3338 | 0.0060 | 0.0014 |
| 20.0000 | 6.9929 | 7.3464 | 0.0058 | 0.0013 |
| 20.1000 | 7.0077 | 7.3588 | 0.0056 | 0.0012 |
| 20.2000 | 7.0224 | 7.3711 | 0.0054 | 0.0012 |

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|---------|--------|--------|--------|--------|
| 20.3000 | 7.0370 | 7.3832 | 0.0052 | 0.0011 |
| 20.4000 | 7.0513 | 7.3951 | 0.0050 | 0.0011 |
| 20.5000 | 7.0655 | 7.4069 | 0.0048 | 0.0010 |
| 20.6000 | 7.0796 | 7.4186 | 0.0046 | 0.0010 |
| 20.7000 | 7.0935 | 7.4301 | 0.0045 | 0.0010 |
| 20.8000 | 7.1073 | 7.4415 | 0.0043 | 0.0009 |
| 20.9000 | 7.1209 | 7.4528 | 0.0042 | 0.0009 |
| 21.0000 | 7.1344 | 7.4639 | 0.0040 | 0.0008 |
| 21.1000 | 7.1477 | 7.4748 | 0.0039 | 0.0008 |
| 21.2000 | 7.1609 | 7.4856 | 0.0037 | 0.0008 |
| 21.3000 | 7.1739 | 7.4963 | 0.0036 | 0.0007 |
| 21.4000 | 7.1868 | 7.5069 | 0.0035 | 0.0007 |
| 21.5000 | 7.1996 | 7.5173 | 0.0033 | 0.0007 |
| 21.6000 | 7.2122 | 7.5276 | 0.0032 | 0.0006 |
| 21.7000 | 7.2247 | 7.5378 | 0.0031 | 0.0006 |
| 21.8000 | 7.2370 | 7.5478 | 0.0030 | 0.0006 |
| 21.9000 | 7.2492 | 7.5577 | 0.0029 | 0.0006 |
| 22.0000 | 7.2613 | 7.5675 | 0.0028 | 0.0005 |
| 22.1000 | 7.2732 | 7.5772 | 0.0027 | 0.0005 |
| 22.2000 | 7.2850 | 7.5867 | 0.0026 | 0.0005 |
| 22.3000 | 7.2967 | 7.5962 | 0.0025 | 0.0005 |
| 22.4000 | 7.3083 | 7.6055 | 0.0024 | 0.0005 |
| 22.5000 | 7.3197 | 7.6147 | 0.0023 | 0.0004 |
| 22.6000 | 7.3310 | 7.6237 | 0.0022 | 0.0004 |
| 22.7000 | 7.3422 | 7.6327 | 0.0022 | 0.0004 |
| 22.8000 | 7.3533 | 7.6416 | 0.0021 | 0.0004 |
| 22.9000 | 7.3642 | 7.6503 | 0.0020 | 0.0004 |
| 23.0000 | 7.3750 | 7.6589 | 0.0019 | 0.0003 |
| 23.1000 | 7.3857 | 7.6675 | 0.0019 | 0.0003 |
| 23.2000 | 7.3963 | 7.6759 | 0.0018 | 0.0003 |
| 23.3000 | 7.4068 | 7.6842 | 0.0017 | 0.0003 |
| 23.4000 | 7.4171 | 7.6924 | 0.0017 | 0.0003 |
| 23.5000 | 7.4274 | 7.7005 | 0.0016 | 0.0003 |
| 23.6000 | 7.4375 | 7.7085 | 0.0016 | 0.0003 |
| 23.7000 | 7.4475 | 7.7164 | 0.0015 | 0.0003 |
| 23.8000 | 7.4574 | 7.7242 | 0.0015 | 0.0002 |
| 23.9000 | 7.4672 | 7.7319 | 0.0014 | 0.0002 |
| 24.0000 | 7.4769 | 7.7395 | 0.0014 | 0.0002 |

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|---------|--------|--------|--------|--------|
| 24.1000 | 7.4865 | 7.7471 | 0.0013 | 0.0002 |
| 24.2000 | 7.4960 | 7.7545 | 0.0013 | 0.0002 |
| 24.3000 | 7.5053 | 7.7618 | 0.0012 | 0.0002 |
| 24.4000 | 7.5146 | 7.7690 | 0.0012 | 0.0002 |
| 24.5000 | 7.5238 | 7.7762 | 0.0011 | 0.0002 |
| 24.6000 | 7.5329 | 7.7833 | 0.0011 | 0.0002 |
| 24.7000 | 7.5418 | 7.7902 | 0.0011 | 0.0002 |
| 24.8000 | 7.5507 | 7.7971 | 0.0010 | 0.0002 |
| 24.9000 | 7.5595 | 7.8039 | 0.0010 | 0.0002 |
| 25.0000 | 7.5681 | 7.8106 | 0.0009 | 0.0001 |
| 25.1000 | 7.5767 | 7.8172 | 0.0009 | 0.0001 |
| 25.2000 | 7.5852 | 7.8238 | 0.0009 | 0.0001 |
| 25.3000 | 7.5936 | 7.8302 | 0.0008 | 0.0001 |
| 25.4000 | 7.6019 | 7.8366 | 0.0008 | 0.0001 |
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| 25.9000 | 7.6420 | 7.8673 | 0.0007 | 0.0001 |
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| 26.4000 | 7.6799 | 7.8962 | 0.0006 | 0.0001 |
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| 26.7000 | 7.7017 | 7.9126 | 0.0005 | 0.0001 |
| 26.8000 | 7.7088 | 7.9179 | 0.0005 | 0.0001 |
| 26.9000 | 7.7158 | 7.9232 | 0.0005 | 0.0001 |
| 27.0000 | 7.7228 | 7.9284 | 0.0005 | 0.0001 |
| 27.1000 | 7.7296 | 7.9336 | 0.0004 | 0.0001 |
| 27.2000 | 7.7364 | 7.9387 | 0.0004 | 0.0001 |
| 27.3000 | 7.7431 | 7.9437 | 0.0004 | 0.0001 |
| 27.4000 | 7.7498 | 7.9486 | 0.0004 | 0.0001 |
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| 27.6000 | 7.7628 | 7.9583 | 0.0004 | 0.0000 |
| 27.7000 | 7.7692 | 7.9631 | 0.0004 | 0.0000 |
| 27.8000 | 7.7756 | 7.9678 | 0.0003 | 0.0000 |

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| 27.9000 | 7.7818 | 7.9725 | 0.0003 | 0.0000 |
| 28.0000 | 7.7881 | 7.9771 | 0.0003 | 0.0000 |
| 28.1000 | 7.7942 | 7.9816 | 0.0003 | 0.0000 |
| 28.2000 | 7.8003 | 7.9861 | 0.0003 | 0.0000 |
| 28.3000 | 7.8063 | 7.9905 | 0.0003 | 0.0000 |
| 28.4000 | 7.8122 | 7.9949 | 0.0003 | 0.0000 |
| 28.5000 | 7.8181 | 7.9992 | 0.0003 | 0.0000 |
| 28.6000 | 7.8239 | 8.0034 | 0.0003 | 0.0000 |
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| 28.8000 | 7.8353 | 8.0118 | 0.0002 | 0.0000 |
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| 31.8000 | 7.9790 | 8.1147 | 0.0001 | 0.0000 |
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| 32.1000 | 7.9909 | 8.1230 | 0.0001 | 0.0000 |
| 32.2000 | 7.9948 | 8.1257 | 0.0001 | 0.0000 |
| 32.3000 | 7.9986 | 8.1284 | 0.0001 | 0.0000 |
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| 32.6000 | 8.0099 | 8.1362 | 0.0001 | 0.0000 |
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| 34.2000 | 8.0638 | 8.1731 | 0.0000 | 0.0000 |
| 34.3000 | 8.0669 | 8.1752 | 0.0000 | 0.0000 |
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| 34.6000 | 8.0759 | 8.1812 | 0.0000 | 0.0000 |
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| 46.3000 | 8.2673 | 8.3019 | 0.0000 | 0.0000 |
| 46.4000 | 8.2681 | 8.3024 | 0.0000 | 0.0000 |
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| 46.8000 | 8.2711 | 8.3041 | 0.0000 | 0.0000 |

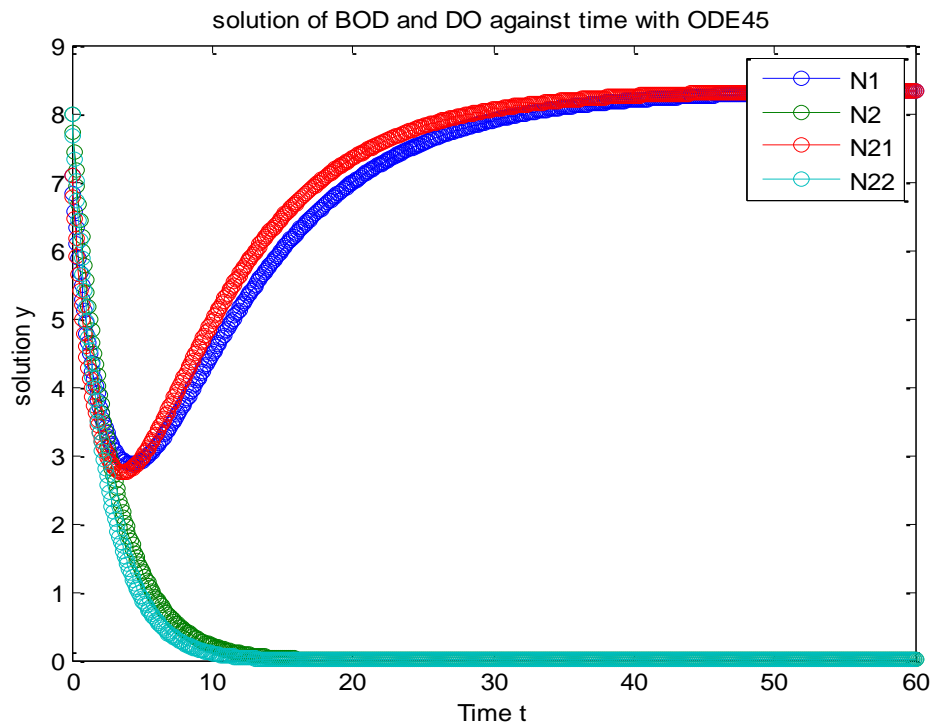
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| 47.4000 | 8.2755 | 8.3065 | 0.0000 | 0.0000 |
| 47.5000 | 8.2762 | 8.3069 | 0.0000 | 0.0000 |
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| 53.8000 | 8.3073 | 8.3237 | 0.0000 | 0.0000 |
| 53.9000 | 8.3076 | 8.3239 | 0.0000 | 0.0000 |
| 54.0000 | 8.3079 | 8.3240 | 0.0000 | 0.0000 |
| 54.1000 | 8.3083 | 8.3242 | 0.0000 | 0.0000 |
| 54.2000 | 8.3086 | 8.3244 | 0.0000 | 0.0000 |
| 54.3000 | 8.3089 | 8.3245 | 0.0000 | 0.0000 |
| 54.4000 | 8.3092 | 8.3247 | 0.0000 | 0.0000 |

| | | | | |
|---------|--------|--------|--------|--------|
| 54.5000 | 8.3095 | 8.3248 | 0.0000 | 0.0000 |
| 54.6000 | 8.3099 | 8.3250 | 0.0000 | 0.0000 |
| 54.7000 | 8.3102 | 8.3252 | 0.0000 | 0.0000 |
| 54.8000 | 8.3105 | 8.3253 | 0.0000 | 0.0000 |
| 54.9000 | 8.3108 | 8.3255 | 0.0000 | 0.0000 |
| 55.0000 | 8.3111 | 8.3256 | 0.0000 | 0.0000 |
| 55.1000 | 8.3114 | 8.3258 | 0.0000 | 0.0000 |
| 55.2000 | 8.3117 | 8.3259 | 0.0000 | 0.0000 |
| 55.3000 | 8.3119 | 8.3260 | 0.0000 | 0.0000 |
| 55.4000 | 8.3122 | 8.3262 | 0.0000 | 0.0000 |
| 55.5000 | 8.3125 | 8.3263 | 0.0000 | 0.0000 |
| 55.6000 | 8.3128 | 8.3265 | 0.0000 | 0.0000 |
| 55.7000 | 8.3131 | 8.3266 | 0.0000 | 0.0000 |
| 55.8000 | 8.3133 | 8.3267 | 0.0000 | 0.0000 |
| 55.9000 | 8.3136 | 8.3269 | 0.0000 | 0.0000 |
| 56.0000 | 8.3139 | 8.3270 | 0.0000 | 0.0000 |
| 56.1000 | 8.3141 | 8.3271 | 0.0000 | 0.0000 |
| 56.2000 | 8.3144 | 8.3273 | 0.0000 | 0.0000 |
| 56.3000 | 8.3147 | 8.3274 | 0.0000 | 0.0000 |
| 56.4000 | 8.3149 | 8.3275 | 0.0000 | 0.0000 |
| 56.5000 | 8.3152 | 8.3276 | 0.0000 | 0.0000 |
| 56.6000 | 8.3154 | 8.3278 | 0.0000 | 0.0000 |
| 56.7000 | 8.3157 | 8.3279 | 0.0000 | 0.0000 |
| 56.8000 | 8.3159 | 8.3280 | 0.0000 | 0.0000 |
| 56.9000 | 8.3161 | 8.3281 | 0.0000 | 0.0000 |
| 57.0000 | 8.3164 | 8.3282 | 0.0000 | 0.0000 |
| 57.1000 | 8.3166 | 8.3284 | 0.0000 | 0.0000 |
| 57.2000 | 8.3168 | 8.3285 | 0.0000 | 0.0000 |
| 57.3000 | 8.3171 | 8.3286 | 0.0000 | 0.0000 |
| 57.4000 | 8.3173 | 8.3287 | 0.0000 | 0.0000 |
| 57.5000 | 8.3175 | 8.3288 | 0.0000 | 0.0000 |
| 57.6000 | 8.3177 | 8.3289 | 0.0000 | 0.0000 |
| 57.7000 | 8.3180 | 8.3290 | 0.0000 | 0.0000 |
| 57.8000 | 8.3182 | 8.3291 | 0.0000 | 0.0000 |
| 57.9000 | 8.3184 | 8.3292 | 0.0000 | 0.0000 |
| 58.0000 | 8.3186 | 8.3293 | 0.0000 | 0.0000 |
| 58.1000 | 8.3188 | 8.3294 | 0.0000 | 0.0000 |
| 58.2000 | 8.3190 | 8.3295 | 0.0000 | 0.0000 |

| | | | | |
|---------|--------|--------|--------|--------|
| 58.3000 | 8.3192 | 8.3296 | 0.0000 | 0.0000 |
| 58.4000 | 8.3194 | 8.3297 | 0.0000 | 0.0000 |
| 58.5000 | 8.3196 | 8.3298 | 0.0000 | 0.0000 |
| 58.6000 | 8.3198 | 8.3299 | 0.0000 | 0.0000 |
| 58.7000 | 8.3200 | 8.3300 | 0.0000 | 0.0000 |
| 58.8000 | 8.3202 | 8.3301 | 0.0000 | 0.0000 |
| 58.9000 | 8.3204 | 8.3302 | 0.0000 | 0.0000 |
| 59.0000 | 8.3206 | 8.3303 | 0.0000 | 0.0000 |
| 59.1000 | 8.3208 | 8.3304 | 0.0000 | 0.0000 |
| 59.2000 | 8.3210 | 8.3305 | 0.0000 | 0.0000 |
| 59.3000 | 8.3212 | 8.3306 | 0.0000 | 0.0000 |
| 59.4000 | 8.3214 | 8.3306 | 0.0000 | 0.0000 |
| 59.5000 | 8.3215 | 8.3307 | 0.0000 | 0.0000 |
| 59.6000 | 8.3217 | 8.3308 | 0.0000 | 0.0000 |
| 59.7000 | 8.3219 | 8.3309 | 0.0000 | 0.0000 |
| 59.8000 | 8.3221 | 8.3310 | 0.0000 | 0.0000 |
| 59.9000 | 8.3222 | 8.3311 | 0.0000 | 0.0000 |
| 60.0000 | 8.3224 | 8.3311 | 0.0000 | 0.0000 |

Trend of the solution trajectory



From the result obtained in the Table displayed on the **impact of temperature variation (Increasing Temperature @ T=28unit)** in the interaction between BOD (IC = 8.0) and DO (IC = 7.1) at an interval of 0(0.1)60 time in hrs, when all model parameter values are fixed ranging from the time interval of 0:0.1:60 in hrs. The BOD and DO initial values here called the IC's on the base time recorded as $BOD_0 = 8.0$ and $DO_0 = 7.1$ due to the pollution of the stream. Furthermore, from the base time, we observed a severe depletion of the DO downstream from a value of 7.1 units DO to a value of 4.0099 units DO for the uncontrol coordinate and 4.4353unit DO for the control (Modified) coordinate at 1.7hr of our experimental time.

In this scenario, above the point of waste water entry (above the DO IC on base day) is classified as the upstream which is called "clean water zone" and is characterized by clear and fresh water containing a stable aquatic environment which is conducive for natural fish, micro-invertebrates and plankton population as DO levels within this zone are near saturation.

However, as the pollution enters the stream, a short zone which is observed from the base day of our experimental time up to 1.7hrs is identified as the "zone of degradation" because of its severe depletion in the DO coordinates downstream. This zone is considered to be turbid as a result of the severe depletion of the DO and as such sunlight is usually reduced with depth in the stream. Moreso, this zone degradation will record a drastic change in chemical characteristics of the stream which is captured in the data been analysed, which include scenarios such as up to a 40% reduction of the DO from the initial condition as observed from the base time up to 1.7hrs with an increase in CO_2 concentration, Nitrogen present in organic form as well as bacterial activities increases. Green and blue algae will be present, fungi will be present, and protozoa (ciliates) will be in relative abundance as well as blood worm.

Again, from the interval of (1.7-8.7) hrs is regarded as a "zone of active decomposition" downstream due to pollution with a critical DO deficit of 2.8682 unit at a critical time at 4.3hrs of our experimental time on the uncontrol coordinates and a critical DO_m deficit of 2.7514unit at a critical time between 3.6-3.7hrs of our experimental time for the control coordinates. The physical characteristics of this period is featured with water that is grey or black in colour, the presence of offensive odours and no light penetration through the stream. As the stream travels within this interval in days, DO and DO_m concentration starts at 40% of the initial condition as seen at the 1.7hrs of our experimental time which drops to the critical DO deficit base on the relative minimum curve as seen at 4.3hrs for the uncontrol coordinates and 3.6-3.7hrs for the control coordinates(DO_m) of our experimental time and as such this interval is a local minimum interval or relative minimum interval with a turning point and its associated critical DO deficit and critical characteristics of gases such as H_2S , C_H4 and NH_3 , which are normally produced as DO is depleted and contributes to the offensive odour problem in the stream.

Most importantly, as DO level drops, bacteria and algae may be the only life form present in the stream column, while other aquatic species both flora and fauna are vulnerable or may tend

to biological extinction or possible migration. Though a slight recovery in the coordinate of the DO at 4.4hrs with $DO = 2.8699$ unit for the uncontrol coordinate and DO_m at 3.8hrs with $DO_m = 2.7543$ for the control coordinate of our experimental time. We observed that after the grey area of active decomposition, there is a relative long interval which starts from 8.7hrs up to 20.00hrs which is the inflexion point (hrs). This interval which occurs between the 8.7-20.00hrs is called “interval of active recovery” up to the point of inflexion. The feature of this interval has chemical characteristics which includes: steady rise in DO concentration from 40% of the initial value of the DO concentration as observed at 4.4hrs and the DO_m concentration as observed at 3.8hrs increased monotonically up the saturation level of the DO. Due to this steady increase in the DO, the CO_2 level and Nitrogen present as NH_3 , and organic form decreases as well. Moreso, biological characteristics within this interval has features such as drastic decrease in the relative abundance of the bacteria present due to external temperature influences and a decrease of the presence of protozoa, blue and green algae as well as decrease of the presence of bloodworm. Most importantly, after this zone or interval of active recovery, we observed another interval starting from the point of inflexion which occur on the 20.0hrs up to 60.0hrs of our experimental time. This interval is called a zone of cleaner water and conducive aquatic environment, the characteristics of this interval is due to intervention of external oxygen, temperature and other meteorological factors. The physical, chemical, and biological characteristics of the stream can be said to have returned to normalcy, and to the conditions present upstream of the pollution source with complete saturation on the 60.0hrs of our experimental time with DO value of 8.3224unit and DO_m value of 8.3311.

However, in the coordinates of the BOD, we observed a monotonic decreasing pattern in the concentration from the base time which depleted drastically down the trend to a saturated BOD at 60.0hrs for both the control and uncontrol coordinates.

This observation is consistent and vital for environmental policy making and decision which will improve the scope of protecting the river banks and aquatic environment as a result of pollution. The information discussed here captures grey area of vulnerability of the aquatic environment and will serve as a data base monitoring system for intervention and mitigation due to the pollution of the stream which will be very useful to the environmental protection agency and other related bodies concerned with pollution.

CONCLUSION

Using the analytical method to study the qualitative characterization of the dynamical system is tasking and did not give an early insight of the expected results and also involved some errors due to approximation, we introduced the core method for this work which is the computational method. Through this method, we were able to predict the relative abundance of the BOD-DO in their interactions over a period of *60hrs at an interval 0:0.1:60 hrs* using MatLab ODE45 numerical scheme. It was observed that there was a decrease in the in the relative

abundance of both coordinates and a point of recovery in the DO coordinates with its DO deficit up to its complete saturation.

The differential equation model for effluents discharged used in this work is very effective in the determination and prediction of the relative abundance of the BOD-DO coordinates over a period of time.

RECOMMENDATION

To researchers who may want to do similar works as this, we recommend that:

The impact of the growth rate should be checked using computational methods.

The impact of varying initial conditions should be predicted using computational methods.

Similar methods should be adopted to study the qualitative behavior of other physiochemical properties over time.

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